



Sensing performance of Pd nanogap supported on an elastomeric substrate in a wide temperature range of -40 to 70 °C

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ABSTRACT

We examined the effect of environmental temperature (-40 to 70 °C) on the hydrogen sensing performance of a Pd nanogap sensor supported on an elastomeric polydimethylsiloxane (PDMS) substrate. Sensing tests were conducted using various sensors with different gap widths, prepared with different tensile strains. All sensors operated in an “On-Off” mode with a rapid response time of ~ 1 s at the operating temperatures. The sensing performance was significantly influenced by the high thermal contraction/expansion properties of the PDMS substrate, depending on the environmental temperature. At subzero temperatures (0 , -20 , and -40 °C), the sensing performance was improved owing to the gap narrowing. At high temperatures (above 40 °C), it decreased owing to the gap broadening. The detection limit was 300 ppm at subzero temperatures but $>1\%$ at high temperatures. The results reveal that the Pd nanogap sensor on PDMS is more suitable for detecting H_2 at subzero temperatures. In addition, the sensor showed excellent reproducibility for hundreds of sensing cycles at 25 °C and -40 °C. Furthermore, the sensor was stable to high humidity (above 70 RH%) at 25 °C. Our study demonstrated that the Pd nanogap sensor on a PDMS substrate is a possible candidate for use as an on-board safety H_2 sensor in hydrogen-electric vehicles.

1. Introduction

Recently, the hydrogen economy has gained increasing attention globally. In particular, the use of hydrogen-electric vehicles is expected to increase in major countries, such as the United States, Germany, China, and Japan, which are the largest global automobile markets expanding the demand for automotive hydrogen sensors. The global automotive hydrogen sensor market is expected to reach USD 17.6 million in 2027 [1]. To avoid the explosion risk of highly flammable H_2 , it is essential to develop a sensor that can detect H_2 leaks sensitively and rapidly. The Department of Energy (DOE) in the United States has provided target specifications for H_2 safety sensors for various applications [2,3]. In particular, it has been reported that on-board safety H_2 sensors in fuel cell vehicles should be operational in the temperature range of -40 to 40 °C and a relative humidity range of 5 – 95% [2,3]. The sensor must also meet other requirements, such as an H_2 detection limit of 0.1% , a response time of less than 1 s for 1% H_2 , and a desired lifetime of 10 years [2,3].

Various types (catalytic, thermal conductivity, electrochemical, resistance-based, work function-based, and optical) of H_2 sensors operating with different sensing mechanisms have been developed and commercially available to date [4]. However, most sensors have an H_2 detection limit greater than 1% and a response time longer than 10 s [4]. The selective detection of H_2 is low, power consumption is high, and sensor fabrication is complicated [4]. Moreover, the lowest operating temperature is -20 °C, which is much higher than the DOE requirement. As a result, existing H_2 sensors do not yet meet all the stringent criteria, and more research is needed to develop sensors that satisfy the target specifications.

Sensing materials are essential for achieving high sensitivity and selectivity. In particular, Pd-based materials have been used extensively for H_2 sensors because they provide high sensitivity and selectivity owing to the high affinity of Pd for H_2 . To achieve high sensitivity and low power consumption, one-dimensional Pd-including nanowires [5,6] and nanotubes [7] have been investigated. In addition, Pd nanoparticles have been functionalized on carbon nanotubes [8,9] and

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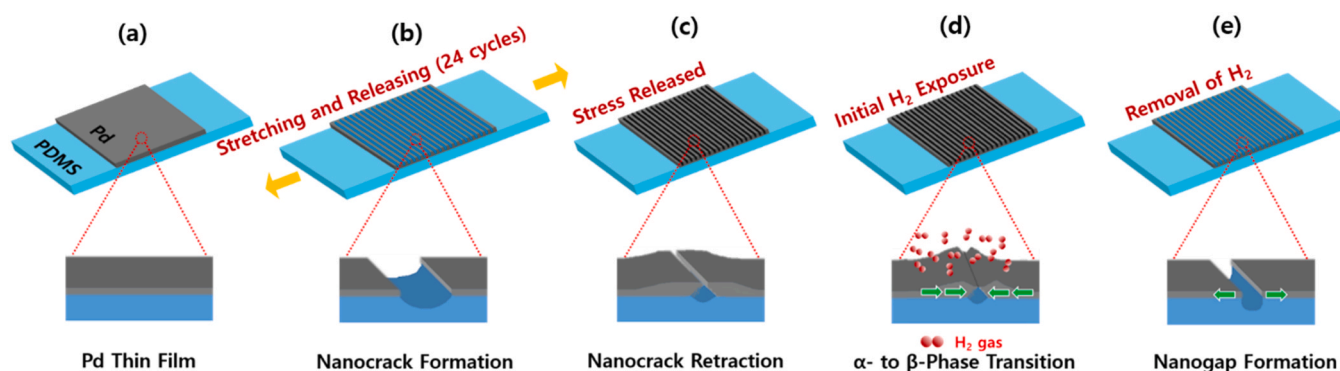


Fig. 1. Schematic of the process of fabrication of nanogaps in a Pd thin film on an elastomeric PDMS substrate by mechanical stretching/compression.

semiconducting nanowires (such as InAs [10] and Si [11,12]). In particular, many studies have investigated various metal oxide semiconductors (such as ZnO [13], NiO [14], TiO₂ [15], In₂O₃ [16], SnO₂ [17], and WO₃ [18]) decorated with Pd nanoparticles [19].

Among the various types of Pd-based H₂ sensors, Pd nanogap-based sensors were first introduced using Pd mesowires comprising Pd nanoparticles [5] to improve the rapid response and short recovery time by applying an “On-Off” sensing mechanism. Subsequently, to improve the sensitivity of Pd mesowires, various electrodeposition methods have been proposed using different lithographic patterning [20,21] and different templates [22,23]. Among the various types of Pd nanogap-based H₂ sensors, the Pd nanogap sensor supported on a poly (dimethylsiloxane) (PDMS) substrate has provided significant advances in H₂ sensing properties, such as high sensitivity, selectivity, and rapid response and recovery times [24,25]. The Pd nanogaps were easily formed on PDMS by simply performing mechanical stretching/compression cycles. H₂ sensing of the Pd nanogap sensors occurs by an “On-Off” mechanism at room temperature. When exposed to H₂, the Pd nanogap sensor is in an “On” state (closed nanogap) because of the volume expansion of Pd by absorbing H atoms. In contrast, upon removing H₂, the sensor is in an “Off” state (open nanogap) because of the volume contraction of Pd by desorbing H atoms. This new approach was achieved using the elastic property of PDMS without lithography, which is very cost-effective. The Pd nanogap sensor on PDMS can detect a lower limit of 0.05% H₂, has a fast response time of 0.67 s for 2% H₂, and can operate at room temperature [24,25].

Since the first report on this sensor [24], there have been many studies, describing reduced detection limits, enhanced sensitivity and selectivity, and improved stability against moisture interference [26–34]. However, all these studies were conducted at room temperature. PDMS has a high coefficient of thermal expansion ($3.4 \times 10^{-4} \text{ }^\circ\text{C}^{-1}$ [35]) compared to other flexible polymers [36,37]. Moreover, the PDMS silicone elastomer retains its flexibility over a temperature range of –45 to 200 °C for an extended time [35]. Thus, using the high coefficient of thermal expansion of PDMS, it is possible to control the Pd nanogap width on the PDMS substrate by controlling the environmental temperature.

In this study, we investigated the effect of environmental temperature on the sensing performances of the Pd nanogap sensors with different gap widths on the PDMS substrate. The width of the Pd nanogap was controlled by applying various tensile strains. The hydrogen sensing tests were performed in a wide range of environmental temperatures ranging from –40 to 80 °C, which is the temperature range specified by the DOE [2,3]. The detection limits and response times were investigated under extreme temperature conditions. We also tested the reproducibility for hundreds of sensing cycles and the sensing stability of the moisture effect for various relative humidities.

2. Materials and methods

2.1. Fabrication of Pd nanogaps on elastomeric PDMS substrate

The elastomeric substrates were prepared using cured PDMS. A silicone elastomer (Sylgard 184, Dow Corning Corp.) of the base material was mixed with a curing agent at an optimized weight ratio of 10:1. The PDMS mixture was kept in a vacuum desiccator at room temperature for 20 min to remove air bubbles and then cured at 75 °C for 4 h on a hot plate. The cured PDMS was cut into pieces with an area of $16 \times 10 \text{ mm}^2$ and a thickness of 1 mm for use as a substrate. A thin Pd film (10 nm, size = $10 \times 10 \text{ mm}^2$) was fabricated on the surface of the PDMS substrate (Fig. 1(a)) using an ultrahigh vacuum direct current (DC) magnetron sputtering system. The base pressure of the DC sputtering chamber was 7.0×10^{-8} Torr. Pd deposition was conducted at a working pressure of 1.2×10^{-4} Torr under 34 sccm of Ar gas flow using a high-purity Pd target (99.99%). The Pd deposition rate was approximately 3.3 \AA/s at an applied power of 20 W.

To make Pd nanocracks on the PDMS substrate, tensile strain was uniformly applied to the specimen of the Pd film/PDMS layers using a micro tensile tester (Linkam Scientific Instruments, TST350). Various nanocracked samples were prepared using different tensile strains of 25%, 50%, 75%, and 100% with a constant tensile velocity of 500 $\mu\text{m/s}$. The tensile strain value was defined as $[(l-l_0)/l_0 \times 100]\%$, where l_0 and l are the initial and final lengths before and after the tensile stress is applied, respectively. The nanocracks were produced during the 24 stretching/releasing cycles at room temperature (Fig. 1(b)). After the stress was released, the nanocracks were retracted and connected to each other (Fig. 1(c)).

To generate Pd nanogaps from the closed nanocracks, the sample was subjected to one cycle of exposure and removal of H₂ gas. When the sample is exposed to H₂, the ends of the broken Pd nanocracks are connected, owing to the volume expansion of Pd because the dissociated H atoms from H₂ molecules are absorbed into the interatomic sites of Pd (α - to β -phase transition [38,39]) (Fig. 1(d)). When H₂ gas is removed, the absorbed hydrogen atoms are rapidly desorbed, resulting in the conversion of PdH_x to Pd (β - to α -phase transition [38,39]), and the Pd ends are relocated relative to the PDMS cracks (Fig. 1(e)). Finally, opened Pd nanogaps are formed on the PDMS substrate. For one cycle of initial exposure, 2% H₂ in N₂ was used.

2.2. Characterization of Pd nanogaps

The distribution of nanogaps on the PDMS substrate, spacing between adjacent nanogaps, and width of nanogaps for the various specimens prepared using different strains were analyzed using optical microscopy (OM, Olympus BX41 M) and scanning electron microscopy (SEM, JEOL JSM-6701F).

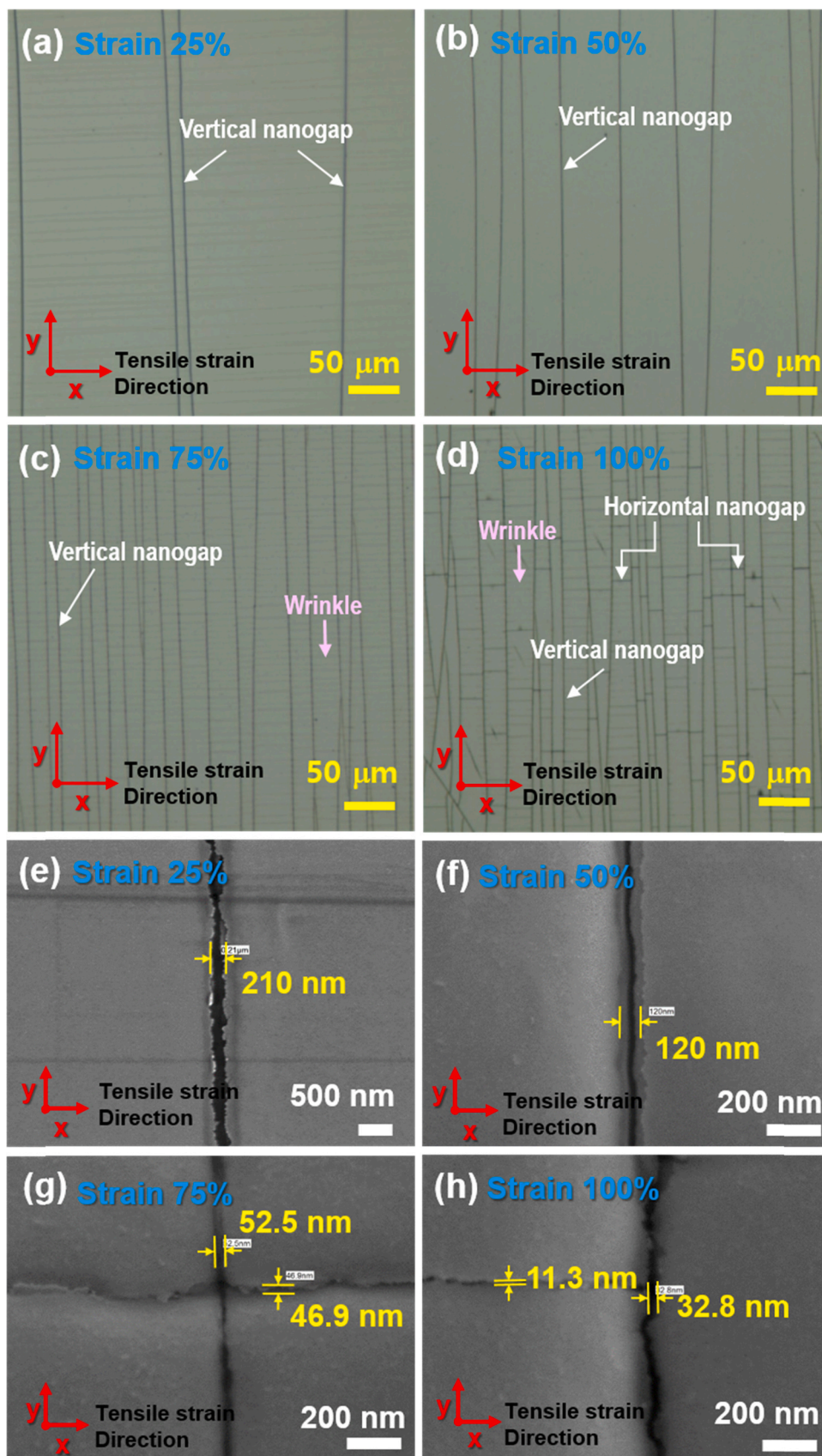


Fig. 2. Top-view optical microscopy; (a)–(d) and scanning electron microscopy; (e)–(h) images of nanogaps formed in a Pd thin film on a PDMS substrate by applying tensile strains of 25%, 50%, 75%, and 100%.

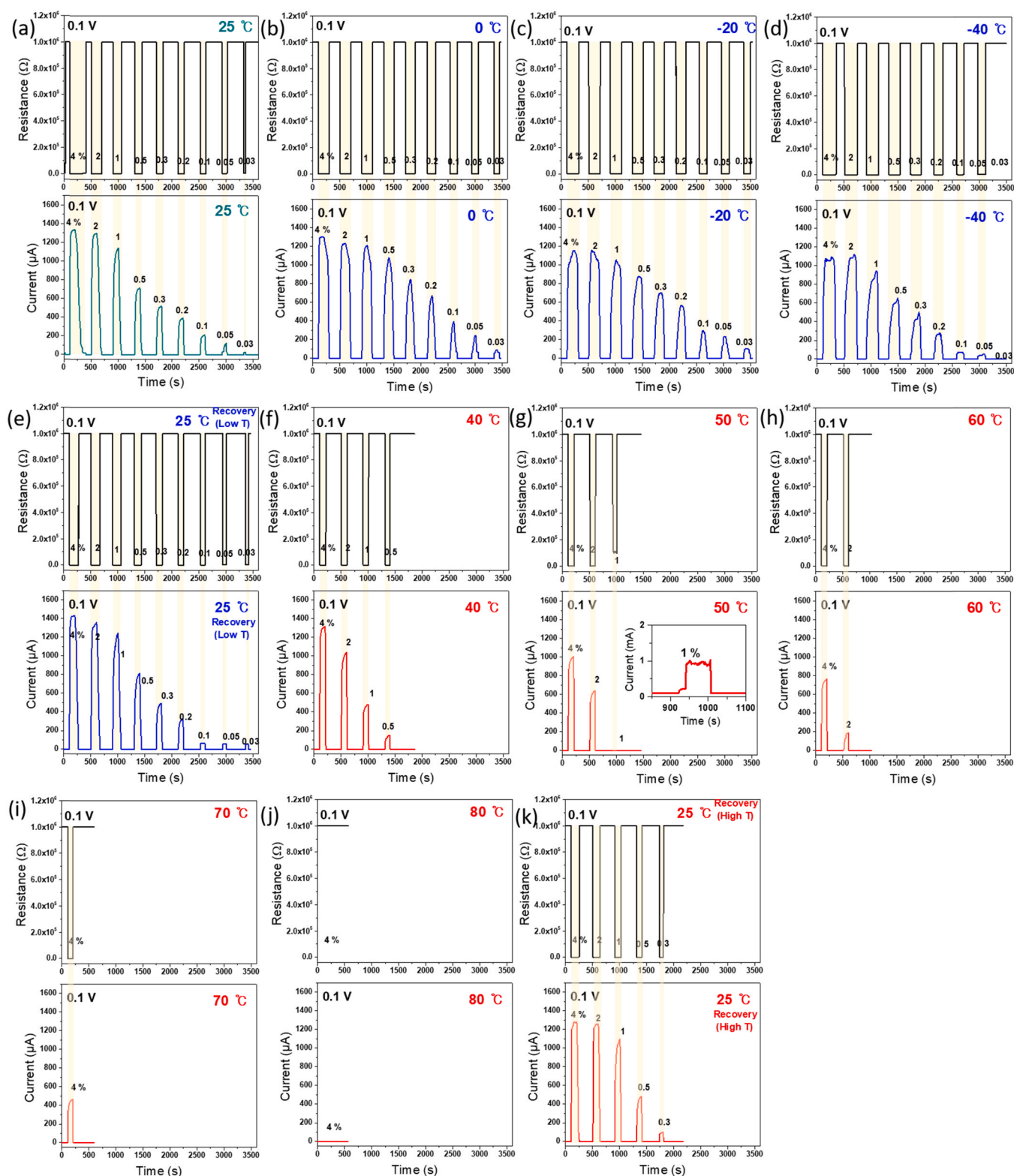


Fig. 3. Real-time electrical responses—resistance (top) and current (bottom)—of the sensor prepared with 75% tensile strain to a gradually decreasing H_2 concentration from 4% to 0.03% at a wide range of operating temperatures from -40 to 80 °C. Electrical currents were measured in the following temperature sequence: (a) 25 °C, (b) 0 °C, (c) -20 °C, (d) -40 °C, (e) 25 °C, (f) 40 °C, (g) 50 °C, (h) 60 °C, (i) 70 °C, (j) 80 °C, and (k) 25 °C.

2.3. Hydrogen sensing measurements

The hydrogen sensing measurements of the as-prepared Pd nanogap sensors fabricated on the PDMS elastomeric substrate were carried out using a microprobe station system (Nextron MPS-PT) equipped with a

source–measure unit (Keithley 6220 and Keithley 2182). A constant voltage of 0.1 V was applied with a time interval of 1 s. The inner volume of the sealed gas chamber was approximately 100 cm³. The chamber had a gas inlet and an outlet. The concentration of H_2 was controlled by mixing a high-concentration H_2 (4%, >99.999%) with N_2

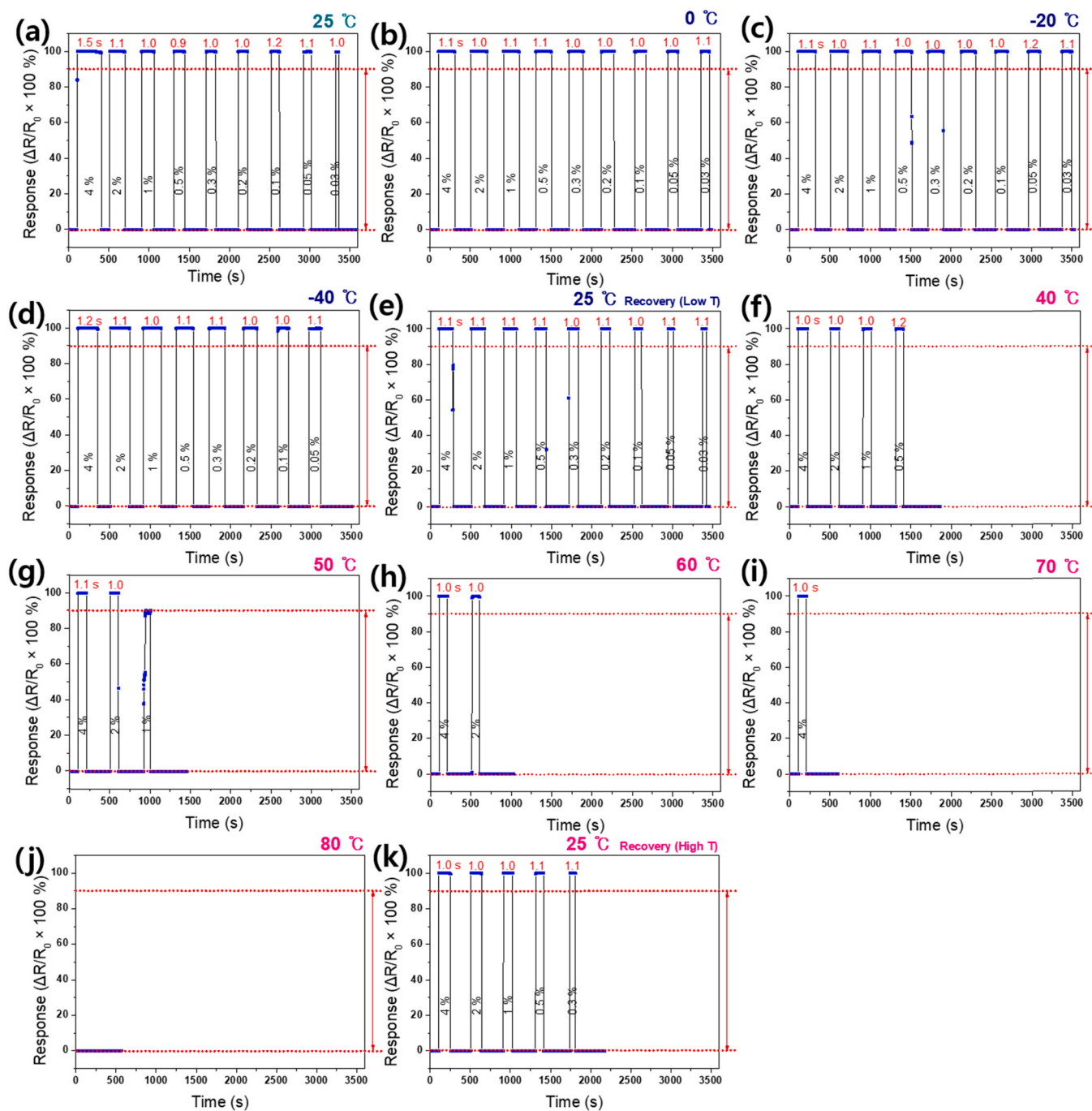


Fig. 4. Response versus time curve for the sensor prepared with 75% tensile strain. The response was converted from the electrical resistance responses. The response time was calculated using a definition of the time to reach 90% of the total change of resistance. The average response times are approximately 1 s for 0.03–4% H_2 at a wide range of low and high temperatures. The time interval between data points is 1 s.

(>99.999%) gas using mass flow controllers (MFCs). Owing to safety concerns, we used N_2 as a carrier gas to control the H_2 concentration under conditions identical to those of the 4% H_2 gas cylinder. H_2 gas mixed with the desired concentration was fed into the gas chamber through the inlet.

To obtain the electrical measurements corresponding to the H_2 sensing properties, a tungsten tip was placed on two electrodes fabricated using silver paste on the surface of a Pd film consisting of a nanogap. The working temperature of the sensor was controlled in the range of -40 to 80 °C by adjusting the temperature of the sample stage in the chamber. The sample stage (18 mm \times 18 mm) made of aluminum nitride was cooled and heated using the Peltier effect. The temperature

was measured using a Pt sensor mounted on the micro probe station.

3. Results and discussion

The distribution of Pd nanogaps on the PDMS substrates formed with different strains was observed using OM. Fig. 2(a)–(d) presents the top-view of the OM images. Twenty-four cycles of tensile strain were applied in the x -direction with strains of 25%, 50%, 75%, and 100% under a constant tensile velocity of 500 $\mu\text{m/s}$. In all strains, vertical nanogaps were produced along the direction of tensile strain. With increasing tensile strain, the spacing between adjacent nanogaps became narrow: ~ 145 μm for 25%, 30 – 85 μm for 50%, 10 – 40 μm for 75%, and

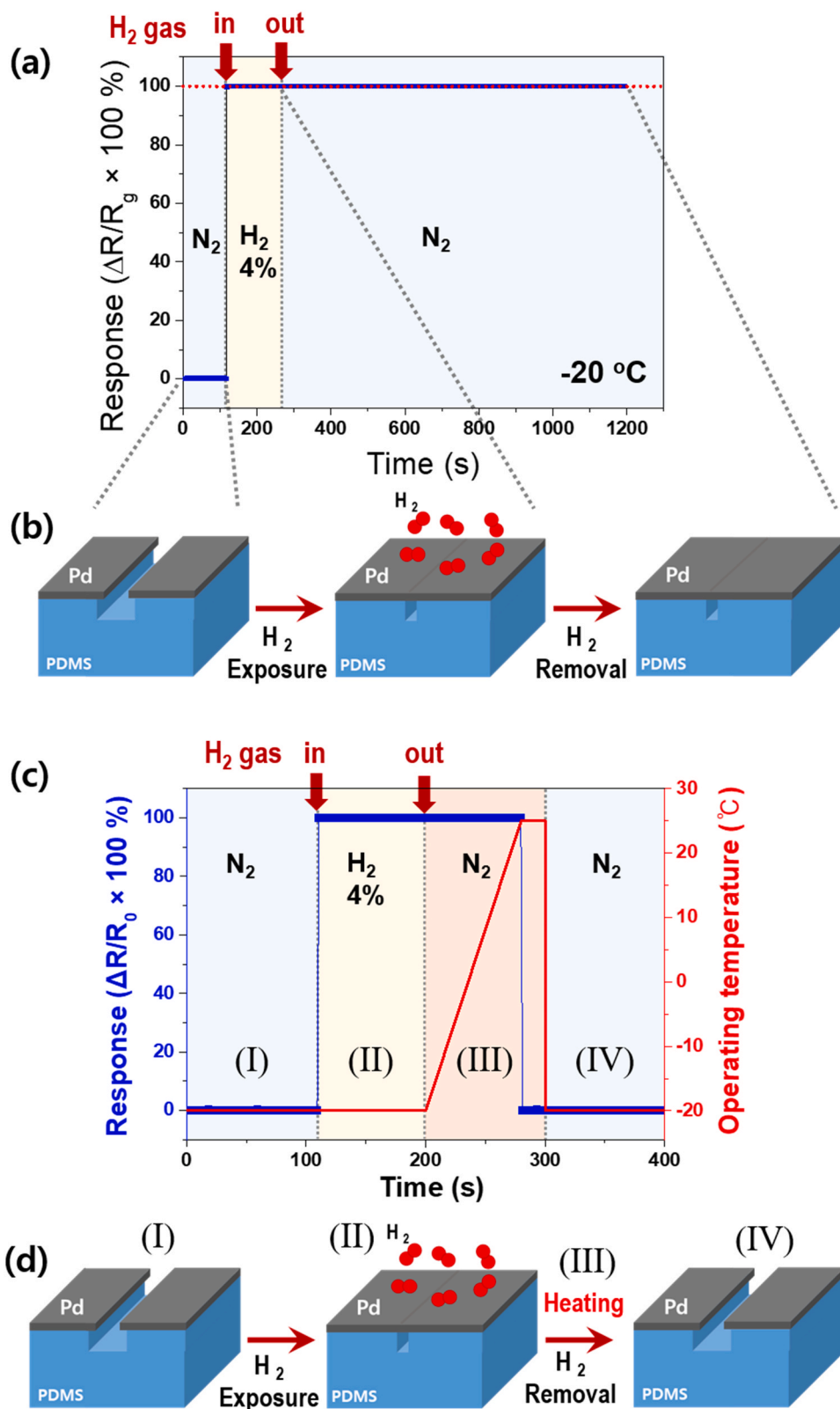


Fig. 5. (a) Response versus time curve of the 75%-strained sensor exposed to 4% H₂ at the subzero operating temperature of -20 °C and (b) illustrations of the nanogap close-open operation of the sensor corresponding to the electrical responses shown in (a); (c) Response versus time curve of the 75%-strained sensor exposed to 4% H₂ at -20 °C. The heating procedure was added when the H₂ gas is removed to open the nanogap. (d) illustrations of the nanogap close-open operation of the sensor corresponding to the electrical responses shown in (c).

10–25 μm for 100%. In addition, at strains of 75% and 100%, horizontal nanogaps were created along the y-direction. Therefore, the density of the formed nanogaps increased with increasing tensile strain.

The average width of the nanogaps formed with different tensile strains was analyzed using SEM. Fig. 2(e)–(h) show representative SEM images of the nanogaps distributed in the specimens; the gap width is

reduced with an increase in strain. The average width of the vertical nanogap was approximately 210 nm for the 25% strain and 120 nm for the 50% strain. The vertical and horizontal nanogaps have widths of ~52 nm and ~47 nm for 75% strain, respectively, and ~33 nm and ~11 nm at 100% strain, respectively. As shown in Figs. 2 and 3, with an increase in the tensile strain, the gap width decreases and more

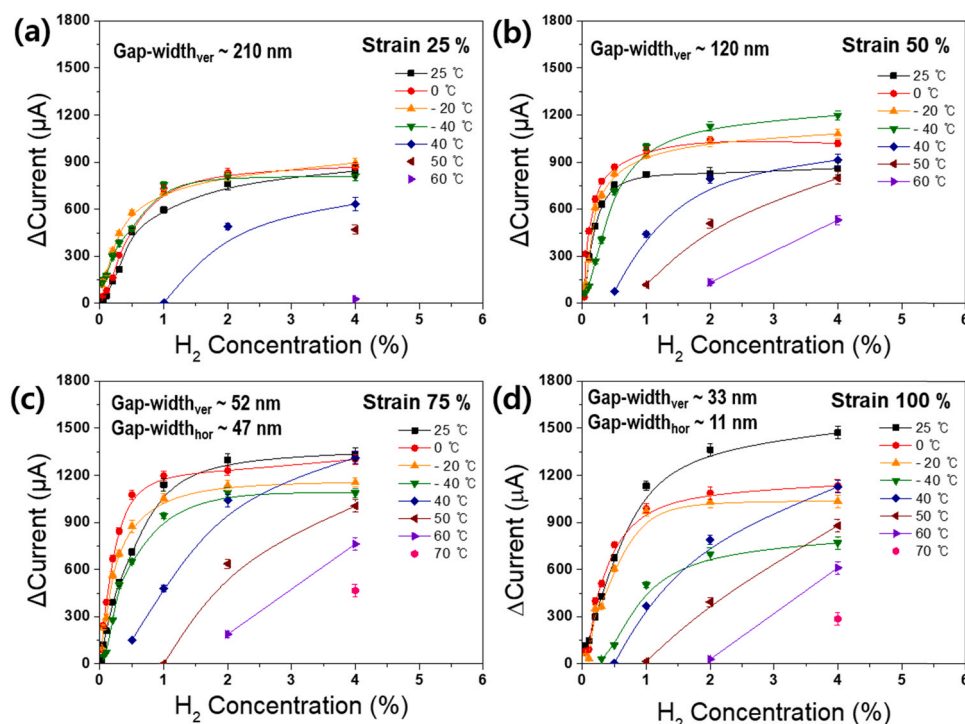


Fig. 6. Current variation versus H_2 concentration curves for various sensors prepared with different tensile strains of (a) 25%, (b) 50%, (c) 75%, and (d) 100% in response to 0.03–4% H_2 at different operating temperatures (–40 to 70 °C). Representative gap widths of vertical and horizontal nanogaps formed in the sensor with different tensile strains are presented in the inset.

nanogaps are formed; this finding is consistent with our previous work [32].

The Hydrogen sensing abilities of the Pd nanogaps on PDMS substrates were examined over a wide range of operating temperatures from –40 to 80 °C. The operating temperature of the sensor was set in two steps: (i) 25 °C → –40 °C → 25 °C and (ii) 25 °C → 80 °C → 25 °C. Real-time electrical responses were measured for various sensors prepared with different tensile strains (25%, 50%, 75%, and 100%). Representative variations of resistance (top) and current (bottom) in real-time under exposure to gradually decreased H_2 concentrations from 4% to 0.03% were presented for the sensor prepared with 75% strain, as shown in Fig. 3. The current variations for the 25%, 50%, and 100% strains are presented in Figs. S1, S3, and S5, respectively, in the Supplementary Material. The on-board safety sensor must be able to detect hydrogen gas at concentrations as low as 0.1–10% [2,3]. In a previous study, the current change in the Pd nanogap sensor on the PDMS substrate indicated the same saturation value for H_2 concentration, from 4% to 10% [24]. Therefore, in this study, we investigated the sensing performance for H_2 concentrations of up to 4%. The results show that the sensor operates in an “On-Off” mode at all the tested temperatures (–40 to 70 °C). The current flow (a significant decrease in resistance) appears when hydrogen is exposed. This is because the nanogaps are closed due to the volumetric expansion of Pd, resulting from hydrogen absorption into the Pd lattice. The maximum width of a nanogap that can be closed via H_2 absorption can be estimated by multiplying the average inter-crack distance and the ratio of lattice expansion [29]. For example, the 75%-strained sensor has an average inter-crack distance of 18 μm ; thus, nanogaps up to 630 nm in width can be closed at room temperature assuming 3.5% lattice expansion, which is the lower boundary of the β PdH_x phase [38,39]. Therefore, the 75%-strained sensor can detect a low H_2 concentration of 300 ppm because the actual width of the nanogap was approximately 50 nm, as shown in Fig. 2(g). Furthermore, the sensor operates in an “On-Off” mode and can detect a low H_2 concentration of 300 ppm at subzero temperatures (0, –20, and –40 °C), as shown in Fig. 3(b)–(d). The detection limit of 300 ppm sufficiently

satisfies the DOE specifications (0.1% H_2) [2,3] even at an extremely low temperature of –40 °C. However, as the operating temperature increased above 40 °C, the current response decreased, and the detectable H_2 concentration increased. The H_2 detection limits were 0.5% at 40 °C and 4% at 70 °C. When the operating temperature was increased to 80 °C, the sensor no longer exhibited a sensing response (Fig. 3(j)). After cooling to 25 °C, it showed a normal “On-Off” sensing reaction on exposure to H_2 (Fig. 3(k)).

The response times of the sensor for the detection of H_2 at various low and high operating temperatures were evaluated from the response curves. The response in time was obtained from the general definition of the resistance change relative to the initial resistance ($|R - R_0|/R_0 \times 100$). Fig. 4 shows the real-time response of the 75%-strained sensor. Those for the 25%, 50%, and 100% strains are presented in Figs. S2, S4, and S6, respectively, in the Supplementary material. As shown in Fig. 4, the response reached 100% for all the H_2 concentrations at the operating temperatures. This is because the sensor operates in an “On-Off” mode. The response time, defined as the time required to reach 90% of the total change in response, was calculated and is presented in Fig. 4. The average response time of the 75%-strained sensor was approximately 1 s for all H_2 concentrations at the operating temperatures. Therefore, the Pd nanogap sensor on the PDMS elastomeric substrate is suitable for detecting leaked hydrogen within a faster time of 1 s, meeting the specifications set by the DOE.

At subzero temperatures (0, –20, and –40 °C), the sensor did not return to the initial open-gap state even after H_2 removal. Fig. 5(a) shows the real-time response for exposure to 4% H_2 at –20 °C. A response of 100%, indicating the flow of the saturation current, was observed even after removing the hydrogen gas. This implies that the closed nanogaps during H_2 exposure do not open at –20 °C even after removing H_2 gas, as illustrated in Fig. 5(b). This can be attributed to the contraction and freezing of the PDMS substrate at the subzero temperature, owing to its high thermal expansion coefficient ($3.4 \times 10^{-4} \text{ }^\circ\text{C}^{-1}$). Therefore, to recover the sensor to the initial open-gap state (stage I in Fig. 5(d)), a heating process had to be included. The resultant response

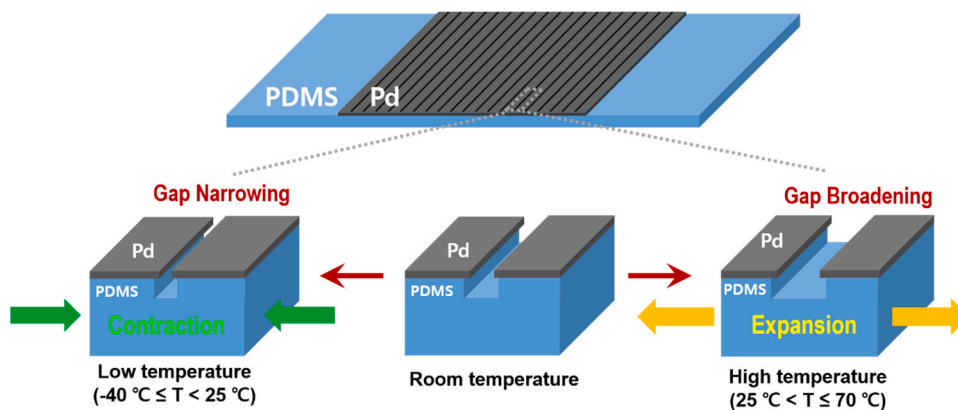


Fig. 7. Schematics of the sensing mechanism for the effect of low and high environmental temperatures on the sensing performance of the Pd nanogap sensor on an elastomeric PDMS substrate.

curve is displayed along with the temperature profile in Fig. 5(c). The sensor in the closed-gap state after H₂ exposure at -20 °C (stage II in Fig. 5(d)) was heated to a temperature of 25 °C with H₂ removal (stage III in Fig. 5(d)) to make the open-gap stage by thermal expansion of PDMS. Subsequently, the operating temperature was cooled back to -20 °C to measure the current response to the next H₂ concentration, and the nanogap remained in the open state, as illustrated in stage III in Fig. 5(d).

To optimize the tensile strain values to fabricate the best sensor that can operate with good sensing ability at various environmental temperatures, the current change, implying the sensing response, was compared in the sensors prepared with different strains (25%, 50%, 75%, and 100%). The current change measured at different operating temperatures (-40 to 70 °C) with decreasing H₂ concentrations is summarized in Fig. 6. At 25 °C, the highest current change is shown in the sensor with 100% strain, owing to the higher density of the nanogap and the smallest gap width (~33 nm for the vertical gap and ~11 nm for the

horizontal gap). However, in the subzero temperature range (0, -20, and -40 °C), the sensing performance of the 100%-strained sensor was significantly reduced, as shown in Fig. 6(d). However, the sensing degradation of the 75%-strained sensor at low temperature was smaller than that of the 100%-strained sensor (Fig. 6(c)). In particular, for the 50%-strained sensor, the sensing performance at subzero temperatures was improved compared to that at 25 °C (Fig. 6(b)). For the 25%-strained sensor, the sensing performance is unchanged over a wide range from room temperature (25 °C) to subzero temperature (-40 °C).

The results in Fig. 6 reveal that the sensing performances at subzero temperatures are strongly affected by the variation in the gap widths of Pd on PDMS with decreasing temperature. As illustrated in Fig. 7, the elastomeric PDMS substrate can shrink at subzero temperatures, and thus the Pd nanogaps may become narrower. The significant sensing degradation at 100% strain can be explained by the fact that the gap smaller than ~40 nm is closed owing to the PDMS contraction at the subzero temperature before H₂ exposure, and the remaining broader

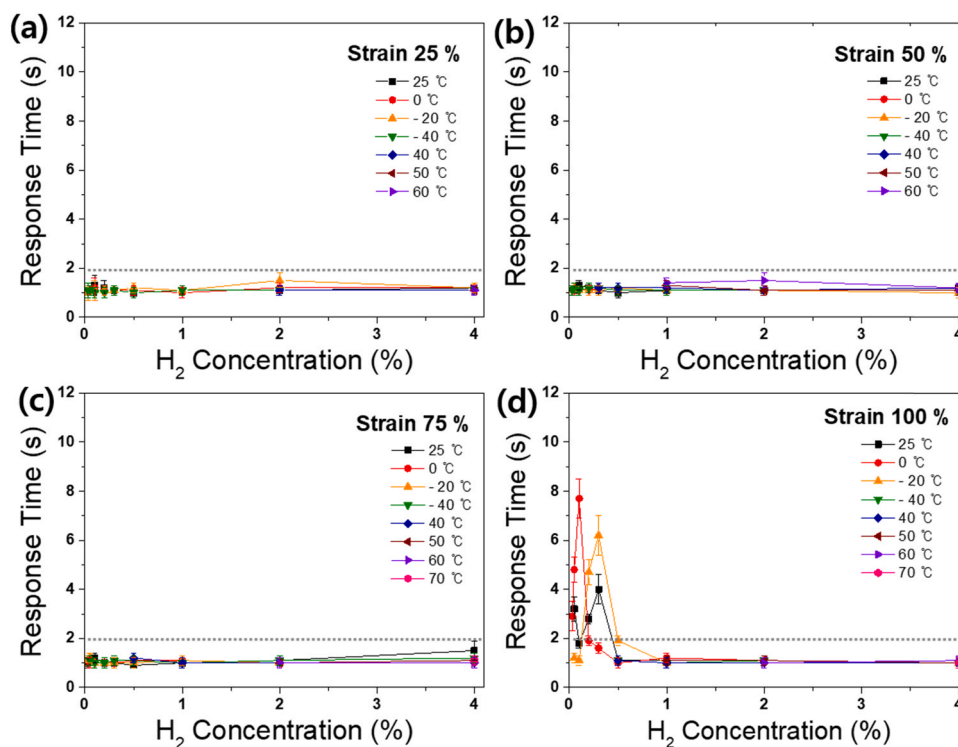


Fig. 8. Sensing response time versus H₂ concentration curves for various sensors prepared with different tensile strains of (a) 25%, (b) 50%, (c) 75%, and (d) 100% in response to 0.03–4% H₂ at different operating temperatures (-40 to 70 °C).

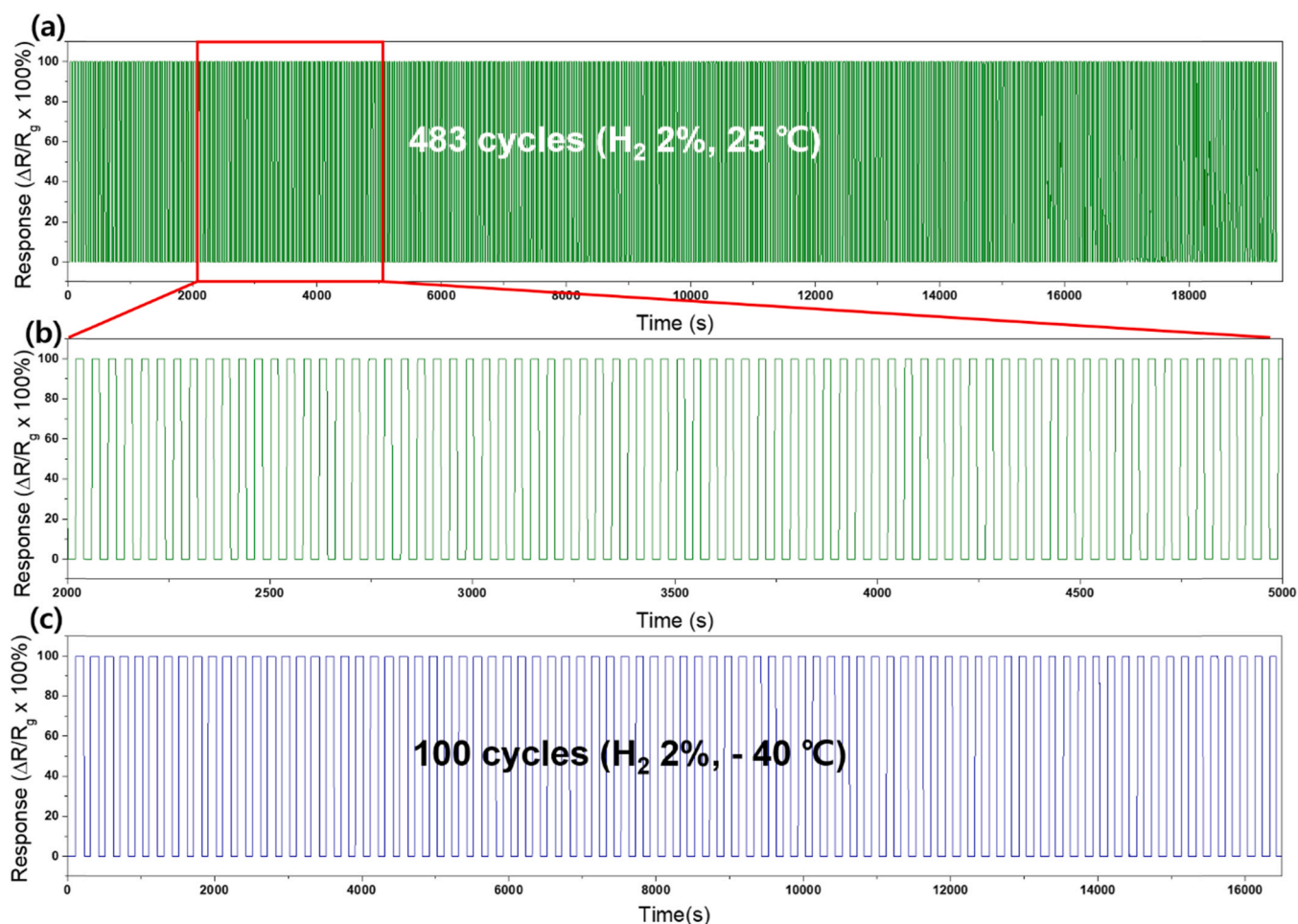


Fig. 9. Sensing reproducibility test of the Pd nanogap sensor on PDMS substrate (75% strain) exposed to 2% H₂ at different temperature environments. (a) Real-time response curves for 483 gas-in and -out cycles at 25 °C, (b) magnified response curves measured between 2000 and 5000 s in (a), and (c) real-time response curves for 100 gas-in and -out cycles at an extremely low temperature of -40 °C.

open gaps take part in H₂ sensing. In the case of the 120 nm width of the 50%-strained sensor, the gap width can be reduced to less than 120 nm at subzero temperatures, and thus the sensing performance can be improved compared to that at room temperature. However, the 210 nm width of the 25%-strained sensor did not affect the low-temperature sensing performance. Fig. 6 also shows that the sensing performance of the Pd nanogap sensor on PDMS is significantly reduced as the operating temperature increases above 25 °C. With decreasing strain (increasing gap width), the current change and the maximum operating temperature decreased. For sensing 4% H₂, the maximum operating temperature was 50 °C for 25% strain and 70 °C for 100% strain. The gap width broadened, owing to the expansion of the PDMS substrate at temperatures above room temperature, as shown in Fig. 7. For example, the change in nanogap length due to the thermal effect was roughly calculated by considering the high thermal expansion coefficient ($3.4 \times 10^{-4} \text{ }^\circ\text{C}^{-1}$ [35]) of PDMS (Supplementary Materials). The calculation was performed on the 75%-strained sensor, which has relatively uniformly distributed nanogaps with similar inter-crack distances. The results indicated that the nanogap lengths of ~ 367 nm and ~ 306 nm can be contracted and expanded when the operating temperature is -40 °C and 70 °C, respectively. In particular, the enlarged nanogap size of ~ 360 nm at 70 °C from ~ 52 nm at room temperature (Fig. 2(g)) can explain the degradation of the sensing performance at a high temperature of 70 °C. Therefore, we concluded that at low and high temperatures, the sensing performances are greatly influenced by the gap width because the gap width varies according to the high thermal

contraction/expansion characteristics of PDMS at those temperatures.

The sensor showing the best sensing performance at the tested temperatures from -40 to 70 °C for a wide range of H₂ concentrations from 4% to 300 ppm is the sensor prepared with 75% strain. In addition, the 75%-strained sensor also showed stable sensing properties after the low- and high-temperature sensing tests compared to the other sensors (Fig. S7). The response times of all sensors prepared with different strains are summarized in Fig. 8. The 25%, 50%, and 75%-strained sensors showed fast response times of less than 2 s under H₂ exposure to varying concentrations at the tested temperatures. However, the 100%-strained sensor shows a slow response time for H₂ concentrations below 0.5% at subzero temperatures. Therefore, the optimized strain value for the best sensing performance and stability in the temperature range from -40 to 70 °C for H₂ concentrations from 4% to 300 ppm is 75%.

Moreover, we tested the reproducibility of the 75%-strained sensor for long-term use at different temperatures of 25 °C and -40 °C by performing hundreds of sensing cycles. Fig. 9(a) shows the real-time response over 483 cycles under 2% H₂ exposure at 25 °C. Fig. 9(b) shows the magnified response curves measured from 2000 to 5000 s in Fig. 9(a). Fig. 9(c) shows the real-time response curves for sensing 2% H₂ over 100 cycles at -40 °C. The response of the Pd nanogap sensor on PDMS remained unchanged at 25 and -40 °C throughout the 483 and 100 (gas-in and -out) cycles, respectively. Therefore, the results reveal that the Pd nanogap sensor supported on PDMS showed an “On-Off” operation during hundreds of sensing cycles regardless of the environmental temperature.

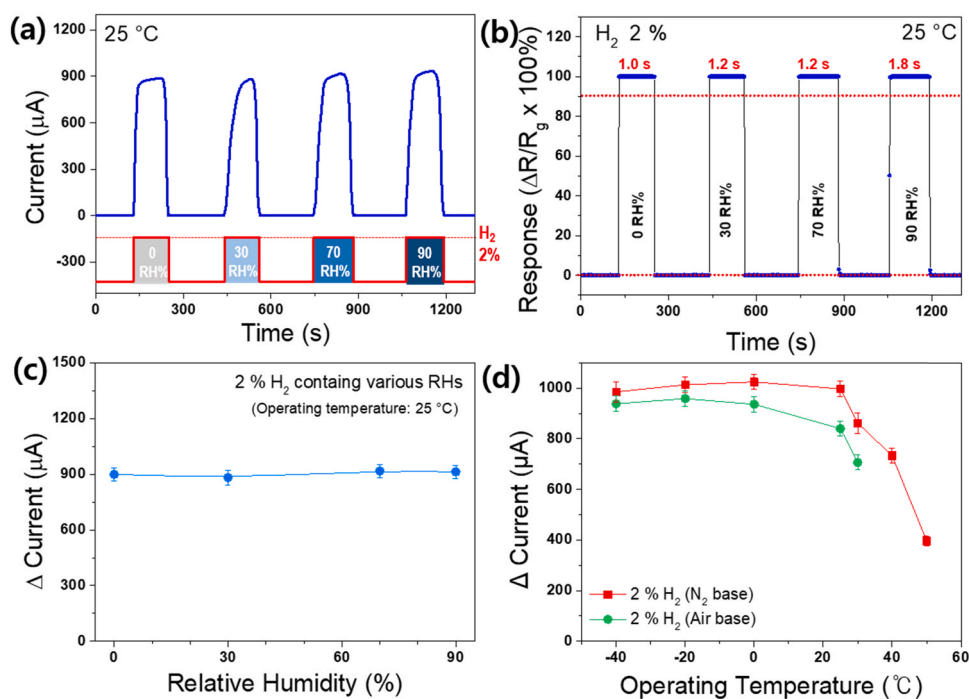


Fig. 10. (a)–(c) Humidity effect of the Pd nanogap sensor on PDMS substrate (75% strain) on the sensing performance to 2% H₂ under different humid conditions (0–90 RH%) at 25 °C: (a) real-time current, (b) real-time response, and (c) dependence of humidity on the current change. (d) comparison of sensing properties at different operating temperatures (–40 to 50 °C) for detecting 2% H₂ in N₂ and synthetic air.

An additional study was performed to investigate the effect of humidity on the sensing performance of the Pd nanogap sensor on the PDMS substrate at room temperature (25 °C) for practical applications. Fig. 10(a) shows the electrical responses of the 75%-strained sensor for the detection of 2% H₂ at different humidity levels (0–90 RH%) at 25 °C. The moist H₂ gas was prepared at room temperature by mixing 2% H₂ with wet N₂, which increased the humidity level from 0 to 90 RH%. The response shows that the sensor operates in an “On-Off” mode under the different humid conditions with rapid response times within 2 s (Fig. 10(b)). In addition, the effect of humidity on the electrical responses was analyzed by comparing the changes in the current shown in Fig. 10(c). The results reveal that the sensor is unaffected by high humidity at 25 °C for sensing 2% H₂.

Furthermore, the H₂-sensing properties of the sensors also need to be measured in synthetic air. However, to investigate the sensing properties of the as-prepared sensors at a relatively high H₂ concentration of 4%, N₂ was used as the balance gas owing to safety concerns. Thus, we further tested the H₂-sensing properties of the 75%-strained sensor in both N₂ and synthetic air. Fig. 10(d) shows the current variation as a function of the operating temperatures (–40 to 50 °C) to detect 2% H₂ in a mixture of N₂ and air. The figure shows that current variations in air, compared with those in an N₂-based atmosphere, remain high at ~95% at –40 °C and ~82% at 30 °C.

4. Conclusion

We investigated the effect of various environmental temperatures (–40 to 80 °C) on the sensing performance of a Pd nanogap sensor supported on an elastomeric PDMS substrate for sensing different H₂ concentrations (0.03–4%). Through the sensing results, the utility of the Pd nanogap on the PDMS sensor as an H₂ safety sensor was verified. The sensor was prepared with different widths of the Pd nanogap by applying different tensile strains (25%, 50%, 75%, and 100%). All sensors operated in an “On-Off” mode with a rapid response time of ~1 s at temperatures ranging from –40 to 70 °C. However, it was found that the sensing performances at low and high temperatures are greatly

influenced by the gap width because the gap width varies owing to the high thermal contraction/expansion characteristics of PDMS at those temperatures. The sensing performance improved at subzero temperatures (0, –20, and –40 °C) owing to gap narrowing, and the detection limit was as low as 300 ppm. However, at high temperatures above 40 °C, the performance was significantly reduced, owing to the gap broadening, and the sensor could detect more than 1% H₂. Consequently, the best sensing performance, such as high current response, fast response time, and low detection limit, at all temperatures from –40 to 70 °C was observed in the sensor with a gap width of ~50 nm (75% strain). In addition, the 75%-strained sensor showed excellent reproducibility for hundreds of sensing cycles at 25 and –40 °C. Furthermore, the humidity effect test showed that the sensor was stable to moisture at 25 °C. Our study demonstrated the potential of the Pd nanogap on an elastomeric PDMS substrate for application to on-board safety H₂ sensors in hydrogen-electric vehicles by controlling the Pd gap width through the thermal contraction and expansion properties of PDMS, depending on the environmental temperature.

CRediT authorship contribution statement

Seyoung Park: Conceptualization, Investigation, Methodology, Validation. **Soo-Min Le:** Methodology, Visualization. **Jin-Kyo Jeong:** Methodology, Formal analysis, Visualization. **Donggu Kim:** Conceptualization, Validation, Visualization. **Hyunsoo Kim:** Validation, Visualization. **Hyun-Sook Lee:** Conceptualization, Validation, Writing – original draft, Writing – review & editing. **Wooyoung Lee:** Supervision.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at [doi:10.1016/j.snb.2021.130716](https://doi.org/10.1016/j.snb.2021.130716).

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